



## Description

### BACKGROUND OF THE INVENTION

#### 1. Field of The Invention

[0001] This invention relates to a system and method for producing a pilot signal in a distortion reduction system, for example in a signal amplification system.

#### 2. Description of Related Art

[0002] Amplifiers often add undesired distortion to a signal, creating an output signal comprising distortion or nonlinear components and the signal component. The distortion includes any undesired signals added to or affecting adversely the input signal. There is therefore a need to devise techniques that can eliminate substantially or reduce significantly the distortion produced by the amplifier.

[0003] Feed-forward correction is routinely deployed in modern amplifiers to improve amplifier linearity with various input patterns. The essence of the feed-forward correction is to manipulate distortion, such as intermodulation (IMD) components, created by the amplifier so that at the final summing point, the distortion cancels out. Due to the unpredictability of input RF carrier pattern as well as the resultant distortion location, a known frequency component, i.e. a pilot signal, is injected in the main signal path with the distortion produced by the amplification process. In feed-forward amplifiers, the feed forward distortion reduction circuitry minimizes the pilot signal along with the distortion. As such, by designing the feed forward distortion reduction circuitry to detect and cancel the pilot signal, the distortion can also be removed.

[0004] The pilot signal is an electrical signal comprising at least one frequency component spectrally located near the frequency band of operation of the electrical circuit. A more complete description of the pilot signal is shown in FIG. 1 which shows the frequency response of a radio frequency (RF) amplifier including the location of the pilot signal. The pilot signal can be near the lower edge of the operating band (e.g., pilot 1) and/or located near the upper edge of the band of operation (e.g., pilot 2). The pilot is positioned a spectral distance of  $\Delta f$  from an edge of the band of operation whose center frequency is  $f_0$ . The electrical characteristics (e.g., amplitude, phase response, spectral content) of the pilot signal are known.

[0005] The feed forward distortion reduction circuitry reduces distortion produced by the RF amplifier by applying the pilot signal to the RF amplifier and making adjustments based on information obtained from the applied pilot signal. FIG. 2 discloses feed-forward correction circuitry 10 and its use of information obtained from the pilot signal to reduce distortion produced by RF amplifier 12. An input signal, for example including at least

one carrier signal, is applied to a splitter 14. The splitter 14 replicates the input signal on a main signal path 16 and a feed forward path 18. The splitter 14 is part of a carrier cancellation loop referred to as loop # 1, which in addition to the splitter 14, comprises gain & phase circuit 20, coupler 22, the RF amplifier 12, delay circuit 24 and couplers 26 and 28. The signal on the main path 16 is applied to gain & phase circuit 20. The output of gain & phase circuit 20 and the pilot signal are applied to the coupler 22. Typically, the amplitude of the pilot signal is much less (e.g., 30 dB less) than the amplitude of the input signal so as not to interfere with the operation of the amplifier 12. The output of the coupler 22 is applied to the amplifier 12 whose output comprises the amplified input signal, the amplified pilot signal and distortion signals produced by the amplifier 12.

[0006] A portion of the output of the amplifier 12 is obtained from the coupler 26 and is combined at the coupler 28 via coupling path 30 with a delayed version of the input signal on the feed forward path 18 to isolate the pilot signal with distortion on the feed forward path 18. The input signal on the feed forward path 18 is sufficiently delayed by delay circuit 24 so that such signal experiences the same delay as the signal appearing at the coupler 28 via the path 30. The resulting error signal contains the distortion produced by the amplifier 12 along with any portion of the carrier signal remaining at the output of the coupler 28 and the pilot signal. The amount of carrier cancellation in the carrier cancellation loop depends on the proper gain and out-of-phase relationship between the two paths from the splitter 14 to the coupler 28.

[0007] The gain & phase circuit 20 adjusts the phase and gain of the input signal according to control signals on control paths 32 and 33 such that the signal appearing at the coupler 28 via the path 30 is substantially the inverse (equal in amplitude but 180° out of phase) of the delayed input signal at the coupler 28. The gain and phase control signals appearing on the control paths 32 and 33 of the gain & phase circuit 20 are derived from the signal at the output of the coupler 28 in a well known manner by sampling the output of the coupler 28 with a coupler 34 and using signal detection and control circuitry 35. In general, the signal detection and control circuitry 35 detects an error signal for the carrier cancellation loop. The error signal represents the amplitude of the carrier signal(s) at point A, and the signal detection and control circuitry 35 attempts to reduce the amplitude of the carrier signal(s) at point A by providing gain and/or phase control signals.

[0008] In this embodiment, the signal detection and control circuitry 35 includes a detector 36, such as a log detector, which produces a signal representing the amplitude of the carrier signal(s) at point A. A filter 38 filters the output of the log detector to produce a DC-type amplitude signal representing the amplitude of the carrier signal(s). The amplitude signal is provided to a nulling circuit 40. In response to the amplitude signal, the nul-

ling circuit 40 provides the control signals on the control paths 32 and 33 to adjust the relative gain and/or phase between the combining signals at the coupler 28 and reduce the carrier signal(s). When the carrier signal(s) is minimized, the carrier signals combined at the coupler 28 substantially cancel each other leaving at the output of the coupler 28 the pilot signal with distortion produced by the amplifier 12. Loop # 1 is thus a carrier cancellation loop which serves to isolate on the feed forward path 18 the pilot signal with distortion produced by the amplifier 12.

[0009] A distortion reduction loop or loop # 2 attempts to reduce the pilot signal on the main signal path 16, thereby reducing the distortion produced by the amplifier 12, using the output of the coupler 28. The pilot signal with distortion on the feed forward path 18 is fed to a gain & phase circuit 42. The output of the gain and phase circuit 42 is fed to amplifier 44 whose output is applied to coupler 46. The coupler 46 combines the amplified pilot signal and distortion on the feed forward path 18 with the signals from the amplifier 12 on the main signal path 16 (carrier signal(s), pilot signal with distortion). A delay circuit 40 on the main signal path 16 delays the signals from the output of the amplifier 12 on the main signal path 16 to experience substantially the same delay as the corresponding signals from the output of the amplifier 12 which pass over the coupling path 30 through the coupler 28 to the coupler 46.

[0010] A coupler 48 provides an error signal representative of the signal at the output of the coupler 46 onto a pilot detection path 50. Because the frequency, amplitude and other electrical characteristics of the pilot signal are known, pilot detection and control circuitry 52 can detect the amplitude of the remaining portion of the pilot signal from the error signal on the pilot detection path 50. The pilot detection and control circuitry 52 determines the amplitude of the pilot signal, and in response to the amplitude of the remaining pilot signal, the pilot detection and control circuitry 52 provides control signals to the phase and gain circuit 42. In general, the pilot detection and control circuitry 52 will detect the pilot signal and use this information to generate control signals onto paths 66 and 68 to cause the gain & phase circuit 42 to adjust the gain and/or phase of the pilot signal on the feed forward path 18 such that the pilot signal on the main path 16 as well as the distortion is substantially the inverse (equal in amplitude but 180° out of phase) of the pilot signal and the distortion on the feed forward path 18 at the coupler 46. The corresponding pilot signals and distortion substantially cancel each other at the coupler 46 leaving the carrier signal(s) at the output of the system. Therefore, loop # 2 is a distortion reduction loop which attempts to cancel the pilot signal to cancel substantially the distortion produced by the amplifier 12.

[0011] In this embodiment, the pilot detection and control circuitry 52 includes pilot receive circuitry 54 which includes a mixer 56 to frequency convert the error

signal on the pilot detection path 50 to lower frequencies and a filter 58 to facilitate detection of the pilot signal by a signal detector 60. The detector 60, such as a log detector, produces a signal representing the amplitude of the signal at the output of the coupler 46. A filter 62 filters the output of the detector 60 to produce a DC-type amplitude signal representing the amplitude of the remaining pilot signal. The amplitude signal is provided to a nulling circuit 64. In response to the amplitude signal, the nulling circuit 64 provides gain and phase control signals on the control paths 66 and 68 to the phase and gain circuit 42. The control signals are provided to adjust the relative gain and/or phase between the pilot signals being combined at the coupler 46 and reduce the remaining pilot signal. The amount of cancellation of the pilot signal indicates the amount of distortion cancellation. When amplitude of the pilot signal is minimized, the pilot signals and distortion combined at the coupler 46 substantially cancel each other at the output of the coupler 46.

[0012] The distortion of the input signal causes power to be generated in adjacent channels or frequencies to corrupt or interfere with signals in the adjacent channels or frequencies, commonly referred to as spectral regrowth or adjacent channel power (ACP). The generation of adjacent channel power is of particular concern in wireless communications systems where adjacent channel power of one channel interferes with other channels or frequency bands. Wireless cellular communications systems comprise a number of base stations, geographically distributed to support transmission and receipt of communication signals to and from wireless units, which can be mobile or fixed, in the geographic region. Each base station handles voice and/or data communications over a particular region called a cell, and the overall coverage area for the cellular system is defined by the union of cells for all of the cell sites, where the coverage areas for nearby cell sites overlap to some degree to ensure (if possible) contiguous communications coverage within the outer boundaries of the system's coverage area.

[0013] In a wireless cellular communications system, a base station and a wireless unit communicate voice and/or data over a forward link and a reverse link, wherein the forward link carries communication signals from the base station to the wireless unit and the reverse link carries communication signals from the wireless unit to the base station. There are many different schemes for determining how wireless units and base stations communicate in a cellular communications system. Multi-user wireless communications systems, such as Code division multiple access (CDMA), wideband CDMA, Time division multiple access (TDMA), Global System for Mobile Communications (GSM) and orthogonal frequency division multiplexing (OFDM), multiple voice and/or traffic channels are combined into a single or multiple carriers. A linear amplifier should be able to react rapidly to transmit power changes and bursty traffic

variations within the transient response specifications in the microsecond and millisecond ranges while providing adequate error cancellation.

[0014] In actual systems, there is rarely an absolute cancellation of the distortion and the pilot signals. Feed forward distortion reduction systems require tight operating tolerances, for example to achieve a 30dB reduction in IMDs, typical feed forward correction system may have a frequency flat response (amplitude deviation over the frequency band of operation) as low as + or - 1dB and phase linearity (phase deviation from a straight line in the frequency band of operation) as low as + or - 1 degree. To obtain this accuracy is difficult. In feed forward distortion reduction systems which use a pilot signal, the amplitude of the pilot signal is typically relatively small at the output of the feed forward distortion reduction system. Accordingly, if the pilot signal is positioned too close to a carrier signal, the pilot signal can be difficult to detect because of the relatively small amplitude of the pilot signal with respect to the amplitude of the carrier signal. Thus, it becomes difficult to detect the pilot signal at the output of the system. If the pilot signal is positioned away from the carrier signal(s) and the resulting IMDs, the pilot signal may be easier to detect but the cancellation of the distortion could suffer because of nonlinearities in the frequency response or phase response of the amplifier over the entire frequency band of operation. To improve detection of the pilot signal at the output of the distortion reduction system, schemes have been developed to scan the in-band frequencies and position the pilot signal at a "quiet" spot in the frequency band of operation which is as close as possible to the active carriers. Such schemes may not react to changing numbers of transmit frequencies.

#### **SUMMARY OF THE INVENTION**

[0015] The present invention involves a distortion reduction system using upstream signal information, such as the carrier frequencies in an input signal, to adjust at least one frequency for a pilot signal to be injected into the distortion reduction system and to be detected at the output of the distortion reduction system, thereby enabling improved distortion reduction of changing input signals. For example, processing circuitry obtains the traffic frequencies making up a signal to be amplified by a feed forward arrangement. Using the traffic frequencies, the processing circuitry determines at least one frequency for a pilot signal, and the processing circuitry tunes a pilot signal generator to the at least one frequency for the pilot signal. The feed forward arrangement receives the signal to be amplified and provides replicas of the signal on a main signal path and on a feed forward path. The pilot signal is injected into the main signal path at the at least one frequency along with the signal to be amplified. The signal and the pilot signal are amplified by an amplifier on the main signal path, resulting in the amplified signal, the amplified pilot signal and distortion

signals produced by the amplifier. A replica of the output of the amplifier is placed on a coupling path and combined with a delayed version of the signal on the feed forward path to isolate a replica of the pilot signal and distortion on the feed forward path. The pilot signal and distortion on the feed forward path are combined with the amplified signal, the amplified pilot and the distortion on the main signal path. A sample of the output is provided to pilot detection circuitry which is tuned by the processing circuitry to detect the pilot signal at the at least one frequency. Depending on the amplitude of the pilot signal at the output, the processing circuitry provides gain and/or phase control signal(s) to adjust the relative phase and/or gain between the combining pilot signals to reduce the amplitude of the pilot signal at the output and thereby to reduce the amplitude of the distortion.

#### **BRIEF DESCRIPTION OF THE DRAWINGS**

[0016] Other aspects and advantages of the present invention may become apparent upon reading the following detailed description and upon reference to the drawings in which:

FIG. 1 shows an example frequency response curve of an RF amplifier showing the frequency within which the amplifier is operating;

FIG. 2 is a block diagram of a feed forward distortion reduction system used for RF amplifiers;

FIGs. 3-6 shows embodiments of a feed forward amplifier distortion reduction system according to the principles of the present invention; and

FIG. 7 shows a flow diagram describing how an embodiment of the feed forward amplifier distortion reduction system operates according to principles of the present invention.

#### **DETAILED DESCRIPTION**

[0017] An illustrative embodiment of a system and method for producing a pilot signal according to the principles of the present invention is described below in a feed forward distortion reduction system. FIG. 3 shows a general block diagram of a feed forward amplifier architecture 80 in which like reference numerals indicate components corresponding to the components of the feed forward amplifier architecture 10 of FIG. 2. In the feed forward amplifier architecture 80, processing circuitry 82 determines the radio channels 84a-n or frequencies to be used, for example in communications between a base station and wireless units. A combiner 85 combines the n radio channels to produce a signal to be amplified by the feed forward arrangement 80. A coupler 86 samples and provides a replica of the input signal to a level detector 87 which produces a signal to the processing circuitry 82 representing the amplitude of the input signal from the combiner 85. The feed forward ar-

rangement 80 receives the signal to be amplified, and a splitter 14 replicates the signal onto a main signal path 16 and a feed forward path 18. The signal on the main signal path 16 is applied to a phase and gain circuit 20, and the output of the phase and gain circuit 20 is applied to an amplifier 12 whose output comprises the amplified signal and distortion signals produced by the amplifier 12. Using the frequencies of the radio channels 84a-n making up the signal, the processing circuitry 82 can determine at least one frequency  $F_P$  for the pilot signal(s). Once the at least one pilot frequency is determined, the processing circuitry 82 can provide a tuning signal 88 to a pilot frequency synthesizer or pilot signal generator 89 to produce a pilot signal at the at least one pilot frequency. Thus, the pilot signal can be generated at a desired location relative to the radio channel frequencies where the pilot signal can be better detected and/or can better reflect the nonlinearities of the amplifier 12 with respect to the active radio channel frequencies.

[0018] In this embodiment, the pilot frequency generator 89 receives a stable reference frequency from a stable reference frequency generator 90. Moreover, the processing circuitry 82 provides a pilot level adjustment signal 91 to a level adjuster 92, such as a variable attenuator. The level adjuster 92 adjusts the level of the pilot signal in response to the pilot level adjustment signal from the processing circuitry 82 which produced the pilot level adjustment signal in response to the amplitude of the signal being provided to the feed forward arrangement 80. A coupler 93 receives the adjusted pilot signal at the at least one pilot frequency  $F_P$  and injects the pilot signal into the main signal path 16 along with the signal to be amplified by the amplifier 12.

[0019] A replica of the output of the amplifier 12, which includes the amplified signal, the amplified pilot signal and distortion, is placed on a coupling path 30 and combined with a delayed version of the signal on the feed forward path 18 to isolate a replica of the amplified pilot and distortion on the feed forward path 18. The pilot signal and distortion on the feed forward path 18 is applied to a gain and/or phase circuit 42 to adjust the amplitude and/or phase of the pilot signal and distortion, and the pilot signal and distortion on the feed forward path 18 is combined with the amplified signal, the amplified pilot signal and the distortion on the main signal path 16 to output the amplified signal with a reduced pilot signal and distortion.

[0020] After the at least one frequency for the pilot signal is identified, the processing circuitry 82 can select the at least one pilot frequency for detection. In this embodiment, the processing circuitry 82 provides a tuning signal 94 to at least one local oscillator (LO) 95 which selects the frequency  $F_{LO}$  of the at least one local oscillator (LO) 95. In this embodiment, the processing circuitry 82 and the LO 95 receive a reference frequency signal from the stable reference frequency generator 90. The selected frequency of the at least one LO 95 is used to frequency convert the pilot signal at the at least one pilot

frequency to facilitate detection of the pilot signal. For example, a coupler 48 samples the amplified signal with reduced pilot signal and distortion after the coupler 46 to provide a replica of the amplified signal and reduced pilot signal and distortion on a pilot signal detection path 96. After being filtered by a band-pass filter 97, the signal on the pilot detection path 96 is provided to a mixer 98 to mix the pilot signal with the frequency from the LO 95. As such, the pilot signal is frequency converted to a frequency  $F_I$ , for example to a lower frequency, where a band pass filter 99, for example a narrowband filter, passes the converted pilot signal while rejecting the other frequencies. The bandpass filter 99 has a center frequency equal to  $F_I$  which is equal to  $F_{LO} - F_P$  or  $F_P - F_{LO}$  and a bandwidth (BW) which can vary depending on the application. The bandwidth can depend on the carrier bandwidth and/or the position of the pilot signal(s) relative to the carrier signal(s), for example a bandwidth of greater than or less than 30 KHz.

[0021] An amplifier 103 amplifies the output of the bandpass filter 96, and a signal detector 100 receives the output of the bandpass filter 99 with the converted pilot signal and produces a signal representing the amplitude of the pilot signal to the processing circuitry 82. In response to the amplitude of the pilot signal at the at least one pilot frequency, the processing circuitry 82 provides gain and/or phase control signal(s) 101 and/or 102 to gain and/or phase circuit 42. The control signals are provided to adjust the relative gain and/or phase between the pilot signals and distortions being combined at the coupler 46 to reduce the pilot signal and thereby the distortion on the main signal path 16. When amplitude of the pilot signal is minimized, the distortion on the feed forward path 18 and the main signal path 16 substantially cancel each other at the output of the coupler 46. As such, the processing circuitry 82 is adjusting the relative phase and/or gain between the pilot signals as well as the distortion products from the main signal path 16 and the feed forward path 18 such that the pilot signals and thereby the distortion products combine at the output to the coupler 46 with a phase difference of about 180 degrees and equal amplitudes.

[0022] To improve the isolation of the pilot signal and distortion on the feed forward path 18, a coupler 34 samples the output to the coupler 28, and signal detection circuitry 104 provides a signal to the processing circuitry 82 that represents the amplitude of the signal at the output to the coupler 28. In response to the signal from the detection circuitry 104, the processing circuitry 82 provides gain and/or phase control signal(s) 106 and/or 108 to gain and/or phase circuit 20. The control signals are provided to adjust the relative gain and/or phase between the signals being combined at the coupler 28 to improve the cancellation of the signal components. As such, the processing circuitry 82 is adjusting the relative phase and/or amplitude between the signal components from the main signal path 16 and the feed forward path 18 such that the signal components combine at the out-

put to the coupler 28 with a phase difference of about 180 degrees and equal amplitudes.

**[0023]** FIG. 4 shows an alternative implementation of a feed forward amplifier architecture 120 in which like reference numerals indicate components corresponding to the components of the feed forward amplifier architectures above. In the feed forward amplifier architecture 120, processing circuitry 122 includes a channel frequency controller 124, such as a digital signal processor (DSP), a microcontroller or other processing circuitry, for assigning radio channels 84a-n coupled to a stand-alone feed forward controller 126, such as a second DSP, microcontroller or other processing circuitry, for controlling the feed forward amplifier architecture 120. In operation, the channel frequency controller 124 assigns the radio channel frequencies 84a-n to be used in communications after being combined and amplified. The channel frequency controller 124 informs the feed forward controller 126 of the channel frequencies from which the feed forward controller 126 determines at least one frequency for a pilot signal. In this embodiment, the channel frequency controller 124 acknowledges the feed forward controller of a change in the radio frequencies with a frequency change acknowledgment 128. The feed forward controller 126 receives the interrupt 128 and sends a handshake signal 130 to the channel frequency controller 124. After which, the feed forward controller 126 receives the new channel frequency information 132 from the channel frequency controller 124. With the new channel frequency information, the feed forward controller 126 determines the at least one frequency for the pilot signal. Accordingly, the tuning signal 88 is provided by the feed forward controller 126 to the pilot signal generator 89 to adjust the at least one pilot signal frequency as well as the tuning signal 94 to the LO 95 for detecting the pilot signal. In response to the amplitude of the detected pilot signal, the feed forward controller 126 provides the gain and/or phase adjustments to the pilot signal and distortion on the feed forward path 18.

**[0024]** FIG. 5 shows an alternative implementation of a feed forward amplifier architecture 140 in which like reference numerals indicate components corresponding to the components of the feed forward amplifier architectures above. In the feed forward amplifier architecture 140, processing circuitry 142, such as a digital signal processor (DSP) or microcontroller, can determine at least one frequency  $F_P$  for the pilot signal generated by the amplifier 12 using the frequencies of the radio channels making up the signal. After the at least one frequency for the pilot signal is identified, the processing circuitry 142 can select the at least one pilot frequency for the pilot signal, and the pilot signal is injected into the main signal path 16 at the at least one pilot frequency  $F_P$ . In this embodiment, the processing circuitry 142 provides tuning signals 144 and 146 to a first local oscillator (LO) 148 and a second local oscillator (LO) 150, respectively, to select respective frequen-

cies  $F_{LO1}$  and  $F_{LO2}$ . The selected frequencies LO1 and LO2 are used to perform a dual frequency conversion of the pilot signal at the least one pilot frequency to facilitate detection of the pilot signal using local oscillator frequencies which are well outside the frequency band of the radio channel frequencies. In the single conversion implementations above, the LO frequency may be in the frequency band or close to the frequency band of the radio frequency channels.

**[0025]** For example, a coupler 48 samples the amplified signal with reduced pilot signal and distortion after the coupler 46 to provide a replica of the amplified signal and the reduced pilot signal and distortion on a pilot detection path 152. After being filtered by a band-pass filter 154, the signal remaining on the pilot detection path 152 is provided to a first mixer 156 to mix the signal on the pilot detection path 152 with the frequency signal from the first LO 148. The first mixer 156 performs a first frequency conversion of the pilot signal to a first intermediate frequency  $F_{I1}$ , for example to a lower frequency, where a low pass filter 158 passes the converted distortion frequency while rejecting higher frequencies. The converted pilot signal (and any remaining signals) is provided to a second mixer 160 to mix the converted pilot signal (and any remaining signals) with the frequency signal LO2 from the second LO 150. The second mixer 160 performs a second frequency conversion of the converted pilot signal to a second intermediate frequency  $F_{I2}$ , for example to an even lower frequency, where a bandpass filter 162, such as a narrowband filter, passes the twice converted pilot signal while rejecting the other frequencies. The bandpass filter 162 can have a center frequency equal to  $F_{I2}$  which is equal to  $F_{LO1} - F_P - F_{LO2}$ ,  $F_P - F_{LO1} - F_{LO2}$ ,  $F_{LO2} - F_{LO1} + F_P$  or  $F_{LO2} - F_P + F_{LO1}$  and a bandwidth (BW) which can vary depending on the application. The bandwidth can depend on the carrier bandwidth and/or the position of the pilot signal(s) relative to the carrier signal(s), for example a bandwidth of greater than or less than 30 KHz.

**[0026]** An amplifier 163 amplifies the output of the bandpass filter 162, and a signal detector 164 receives the output of the bandpass filter 162 with the pilot signal and produces a signal representing the amplitude of the pilot signal to the processing circuitry 142. In response to the amplitude of the pilot signal at the at least one pilot frequency, the processing circuitry 142 provides gain and/or phase control signal(s) 101 and/or 102 to gain and/or phase circuit 42. The control signals are provided to adjust the relative gain and/or phase between the signals being combined at the coupler 46 to reduce the pilot signal and thereby the distortion on the main signal path 16. When amplitude of the pilot signal is minimized, the pilot signal and distortion on the feed forward path 18 and the main signal path 16 substantially cancel each other at the output of the coupler 46. As such, the processing circuitry 142 is adjusting the relative phase and/or gain between the pilot signals as well as the distortion products from the main signal path 16 and the

feed forward path 18 such that the pilot signals and distortion products combine at the output to the coupler 46 with a phase difference of about 180 degrees and equal amplitudes.

[0027] In addition to the embodiments described above, alternative configurations of the feed forward amplifier system according to the principles of the present invention are possible which use variations or portions of the above described system. For example, FIG. 6 shows an alternative implementation of a feed forward amplifier architecture 180 in which like reference numerals indicate components corresponding to the components of the feed forward amplifier architectures above. In the feed forward amplifier architecture 180, processing circuitry 182 includes a channel frequency controller 184, such as a digital signal processor (DSP) or a microcontroller, for assigning radio channels 84a-n coupled to a stand-alone feed forward controller 186, such as a second DSP or microcontroller, for controlling the feed forward amplifier architecture 180. Additionally, the distortion signal at the output of the feed forward amplifier system 180 is detected by performing a dual frequency conversion of the distortion signal as described above for FIG. 5. In operation, the channel frequency controller 184 assigns the radio channel frequencies 84a-n to be used in communications after being combined and amplified. The channel frequency controller 184 informs the feed forward controller 186 of the channel frequencies from which the feed forward controller 186 determines the at least one pilot frequency for the pilot signal using the radio channel frequencies. The feed forward controller tunes the pilot signal generator 89 to the at least one pilot frequency and provides control signals to detect the pilot signal at the at least one pilot frequency. In this embodiment, the channel frequency controller 184 acknowledges the feed forward controller 186 of a change in the radio frequencies with a frequency change acknowledgment 188. The feed forward controller 186 receives the interrupt 188 and sends a handshake signal 190 to the channel frequency controller 184. After which, the feed forward controller 186 receives the new frequency channel information 192 from the channel frequency controller 184.

[0028] The feed forward controller 186 determines at least one pilot frequency  $F_p$  for the pilot signal using the frequencies of the radio channels making up the signal. After the at least one frequency for the pilot signal is identified, the feed forward controller 186 can re-tune the pilot signal generator 89 and select the at least one pilot frequency for detection. In this embodiment, the feed forward controller 186 provides tuning signals 144 and 146 to a first local oscillator (LO) 148 and a second local oscillator (LO) 150, respectively, to select respective frequencies  $F_{LO1}$  and  $F_{LO2}$ . The selected frequencies LO1 and LO2 are used to perform the dual frequency conversion of the at least one pilot frequency to facilitate detection of the pilot signal. In response to the

amplitude of the pilot signal after the coupler 46, the feed forward controller 186 provides phase and/or gain signals 101 and/or 102 to phase and gain circuit 42 to reduce the amplitude of the pilot signal and thereby the distortion at the output.

[0029] FIG. 7 shows a flow diagram describing how an embodiment of the feed forward amplifier system operates to provide phase and/or amplitude adjustments in response to the amplitude of the at least one pilot signal. Embodiments of the flow diagram can operate in the processing circuitry 82 (FIG. 3), 122 (FIG. 4), 142 (FIG. 5) and 182 (FIG. 6) above or portions thereof. In block 200, the  $n$  transmit frequencies or radio channels are stored in a memory, for example in a data bin. In the implementation using a stand-alone feed forward controller 126 (FIG. 4) or 186 (FIG. 6), the feed forward controller receives the  $n$  radio frequencies from the channel frequency controller 124 (FIG. 4) or 184 (FIG. 6). At block 202, a decision is made as to whether the number  $n$  of radio frequency channels is greater than or equal to 2.

[0030] If the number of radio frequency channels is greater than or equal to 2, the processing circuitry obtains the lowest frequency channel  $F_L$  at block 204. The processing circuitry determines a first pilot frequency  $F_p = F_L - \Delta f_p$  at block 206 where  $\Delta f_p$  is a desired frequency offset value used to position the pilot signal a certain distance lower than the lowest carrier signal or radio channel. The frequency offset value can vary depending on the number of radio channels, the desired performance, the existence of gaps between radio channels within the frequency band of operation and/or the particular application. For example, the frequency offset can be greater than less than or about the carrier bandwidth for the particular application, for example bandwidth can vary about 30KHz for TDMA, about 200KHz for wideband TDMA, about 1.225 MHz for CDMA, about 4.05 MHz for wideband CDMA and about 200 KHz for Global System for Mobile Communications (GSM).

[0031] At block 208, the processing circuitry tunes the pilot generator to the appropriate frequency value  $F_p$  for the pilot signal. The processing circuitry determines the appropriate frequency for the LO(s) and programs the LO(s) such that the pilot frequency is converted to fall within the center frequency of the narrowband bandpass filter for detection by the detection circuitry.

[0032] At block 210, the processing circuitry proceeds to a tuning subroutine 212 where the relative amplitude and phase is adjusted between the combining distortion signals to obtain gain and phase values producing a reduced pilot signal. For example, at block 214, the amplitude of the pilot signal at the pilot frequency is detected at the output as represented by a voltage value  $V_{det}$ . A repetitive loop is established at block 216 where count  $= m$  to 1. In the loop at block 218, the processing circuitry provides phase control signals to a variable phase shifter to adjust the relative phase between the pilot signals combining at the coupler 46. The relative phase for the

pilot signals is adjusted so the resulting amplitude level of the pilot signals at the output  $V_{\text{new1}} < V_{\text{det}}$ . At block 220, the processing circuitry provides amplitude or gain control signals to a variable attenuator to adjust the relative amplitude between the pilot signals combining at the coupler 46. The relative amplitude between the pilot signals is adjusted so the resulting amplitude level of the pilot signal at the output  $V_{\text{new2}} \leq V_{\text{new1}}$ . The detected pilot signal amplitude level variable  $V_{\text{det}}$  is set to the value  $V_{\text{new2}}$  at block 222, and the loop counter COUNT is decremented by one at block 224. If the counter COUNT=0 as determined at block 226, the processing circuitry returns at block 228 to the block which called the tuning subroutine. Otherwise, the processing circuitry loops back up to the block 218.

**[0033]** When the tuning subroutine returns from being called at the first tuning point (TP1) of block 210, the processing circuitry stores the phase and amplitude adjustment values at block 230 for the first pilot signal. At block 232, the processing circuitry retrieves the highest channel frequency  $F_H$ . In this embodiment, the processing circuitry then determines a second pilot signal  $F_p = F_L + \Delta f_p$  at block 234 where  $\Delta f_p$  is a desired frequency offset value used to position the pilot signal a certain distance lower than the lowest carrier signal or radio channel. The frequency offset value can vary depending on the number of radio channels, the desired performance, the existence of gaps between radio channels within the frequency band of operation and/or the particular application. For example, the frequency offset can be greater than less than or about the carrier bandwidth for the particular application, for example bandwidth can vary about 30KHz for TDMA, about 200KHz for wideband TDMA, about 1.225 MHz for CDMA, about 4.05 MHz for wideband CDMA and about 200 KHz for Global System for Mobile Communications (GSM).

**[0034]** At block 236, the processing circuitry tunes the pilot generator to the appropriate pilot signal frequency. The processing circuitry also determines the appropriate frequency value(s) for the corresponding LO(s) and programs the LOs such that the second pilot signal is converted to fall within the center frequency of the narrowband bandpass filter for detection by the detection circuitry. At block 238, the processing circuitry calls or proceeds to the tuning subroutine described above (block 212) for the second tuning point (TP2) associated with the second pilot signal. As described above for the first tuning point (TP1), the processing circuitry returns from the tuning subroutine with amplitude and phase adjustment values of the second tuning point which are stored at block 240. As such, the processing circuitry has tuning points which provide reduced amplitude for the first pilot signal associated with the lowest channel frequency and for the second pilot signal associated with the highest channel frequency. To provide overall improved performance, this embodiment of the processing circuitry averages the phase and amplitude adjustment values for the tuning points TP1 and TP2 to pro-

vide the new tuning point  $TP = (TP1 + TP2) / 2$  at block 242. After, the processing circuitry can proceed to block 244 to perform other tasks and/or wait for a change in the radio frequency channels.

**[0035]** If at block 202 the number  $n$  of radio channel frequencies is equal to one, the radio channel frequency  $F_{TX}$  is retrieved at block 246. The processing circuitry determines a first pilot frequency  $F_p = F_{TX} - \Delta f_p$  at block 248 where  $\Delta f_p$  is a desired frequency offset value used to position the pilot signal a certain distance from the carrier signal or radio channel. The frequency offset value can vary depending on the desired performance, the position of the radio channel within the frequency band of operation and/or the particular application. For example, the frequency offset can be greater than less than or about the carrier bandwidth for the particular application, for example bandwidth can vary about 30KHz for TDMA, about 200KHz for wideband TDMA, about 1.225 MHz for CDMA, about 4.05 MHz for wideband CDMA and about 200 KHz for Global System for Mobile Communications (GSM).

**[0036]** At block 250, the processing circuitry tunes the pilot generator to the appropriate frequency value  $F_p$  for the pilot signal. The processing circuitry determines the appropriate frequency for the LO(s) and programs the LO(s) such that the pilot frequency is converted to fall within the center frequency of the narrowband bandpass filter for detection by the detection circuitry. At block 252, the processing circuitry proceeds to a tuning subroutine 212 where the relative amplitude and phase is adjusted between the combining pilot signals to obtain gain and phase values producing a reduced pilot signal at the coupler 46. When the tuning subroutine returns from being called at the first tuning point (TP1) of block 252, the processing circuitry stores the phase and amplitude adjustment values at block 254 for the first pilot signal. In this embodiment, the processing circuitry then determines a second pilot signal  $F_p = F_L + \Delta f_p$  at block 256 where  $\Delta f_p$  is a desired frequency offset value used to position the pilot signal a certain distance higher than the radio channel. The frequency offset value can vary depending on the desired performance, the position of the radio channel within the frequency band of operation and/or the particular application. For example, the frequency offset can be greater than less than or about the carrier bandwidth for the particular application, for example bandwidth can vary about 30KHz for TDMA, about 200KHz for wideband TDMA, about 1.225 MHz for CDMA, about 4.05 MHz for wideband CDMA and about 200 KHz for Global System for Mobile Communications (GSM).

**[0037]** At block 236 as described above, the processing circuitry tunes the pilot generator to the appropriate pilot signal frequency. The processing circuitry also determines the appropriate frequency value(s) for the corresponding LO(s) and programs the LO(s) such that the second pilot signal is converted to fall within the center frequency of the narrowband bandpass filter for detec-



tion by the detection circuitry. At block 238, the processing circuitry calls or proceeds to the tuning subroutine described above (block 212) for the second tuning point (TP2) associated with the second pilot signal. As described above for the first tuning point (TP1), the processing circuitry returns from the tuning subroutine with amplitude and phase adjustment values of the second tuning point which are stored at block 240. As such, the processing circuitry has tuning points which provide reduced amplitude for the first pilot signal associated with the lowest channel frequency and for the second pilot signal associated with the highest channel frequency. To provide overall improved performance, this embodiment of the processing circuitry averages the phase and amplitude adjustment values for the tuning points TP1 and TP2 to provide the new tuning point  $TP = (TP1 + TP2) / 2$  at block 242. After, the processing circuitry can proceed to block 244 to perform other tasks and/or wait for a change in the radio frequency channels.

[0038] In addition to the embodiment described above, alternative configurations of the amplifier distortion reduction system according to the principles of the present invention are possible which omit and/or add components and/or use variations or portions of the described system. For example, the above embodiments are described in a feed forward arrangement, but other embodiments are possible which provide relative gain and/or phase adjustments between combining pilot signals based on the amplitude of the detected pilot signal which is at a frequency determined by the radio frequency channels being amplified. Depending on the application, the gain and/or phase circuitry can be positioned in different locations and/or paths within the feed forward amplifier arrangement. For example the gain and phase adjustment circuit 20 could be located on the path 18 before the coupler 28; the gain and phase adjuster 42 could be located on the path 16 after the coupler 26; or the gain and phase adjustment circuitry 20 and 42 could be located at both locations. Furthermore, the distortion reduction system has been described using a particular example of determining the pilot signal frequency or frequencies using the upstream signal information. Other manners of determining the pilot signal frequency or frequencies can be used which use upstream signal information.

[0039] The distortion reduction system can be implemented in application specific integrated circuits, software-driven processing circuitry, firmware or other arrangements of discrete components as would be understood by one of ordinary skill in the art with the benefit of this disclosure. What has been described is merely illustrative of the application of the principles of the present invention. Those skilled in the art will readily recognize that these and various other modifications, arrangements and methods can be made to the present invention without strictly following the exemplary applications illustrated and described herein and without departing from the spirit and scope of the present inven-

tion.

## Claims

1. A method of producing an amplified signal, said method

### CHARACTERIZED BY:

determining using upstream signal information at least one frequency for a pilot signal; and placing said pilot signal with a signal to be amplified.

2. The method of claim 1 CHARACTERIZED BY:

detecting an amplitude of said pilot signal; and providing gain and/or phase adjustments based on said amplitude of said pilot signal.

3. The method of claim 1 CHARACTERIZED BY:

splitting a signal to be amplified onto a main signal path (16) and a feed forward path (18); amplifying said signal on said main signal path (16) to produce an amplified signal with distortion and said pilot signal on said main signal path (16);

sampling said amplified signal with said distortion and said pilot signal to obtain a replica of said amplified signal with said distortion and said pilot signal on a coupling path (30); combining said signal on said feed forward path (18) with said replica of said amplified signal with said distortion and said pilot signal on said coupling path (30) to produce said pilot signal and said distortion on said feed forward path (18);

applying said pilot signal and said distortion on said feed forward path (18) to a gain and/or phase circuit (42) to adjust the amplitude and/or phase of the distortion and said pilot signal on said feed forward path (18);

combining said pilot signal and distortion on said feed forward path (18) with said amplified signal with said distortion and said pilot signal on said main signal path (16) to output the amplified signal with reduced distortion and said pilot signal;

wherein said detecting includes detecting said amplitude of said pilot signal on said main signal path (16) after said combining; and wherein said providing includes providing gain and/or phase adjustments at said applying based on said amplitude of said pilot signal.

4. The method of claim 2 CHARACTERIZED IN THAT said detecting includes:

obtaining a replica of said amplified signal with said distortion and said pilot signal on a pilot detection path (96);  
 frequency converting said amplified signal with said distortion and said pilot signal on said pilot detection path (96);  
 filtering after frequency converting said amplified signal with said distortion and said pilot signal on said pilot detection path (96) to attenuate said amplified signal while retaining said distortion and said pilot signal; and  
 detecting the amplitude of said pilot signal.

5. The method of claim 4 **CHARACTERIZED IN THAT** said detecting includes:

tuning at least one local oscillator (LO) (95) to at least one LO frequency;  
 mixing said pilot signal with said at least one LO frequency to produce said pilot signal at an intermediate frequency; and  
 filtering said pilot signal using a bandpass filter (99) having said intermediate frequency as said center frequency of said bandpass filter (99).

6. The method of claim 5 **CHARACTERIZED IN THAT** said detecting includes:

tuning a first local oscillator (LO) (148) to a first LO frequency and a second LO (150) to a second LO frequency;  
 mixing said pilot signal with said first LO frequency to produce said pilot signal at a first intermediate frequency; and  
 mixing said pilot signal at said first intermediate frequency with said second LO frequency to produce said pilot signal at a second intermediate frequency; and  
 filtering said pilot signal using a bandpass filter (162) having said second intermediate frequency as said center frequency of said bandpass filter (162).

7. A distortion reduction system **CHARACTERIZED BY:**

processing circuitry (82) configured to receive upstream signal information and to determine at least one frequency for a pilot signal; and  
 pilot generation circuitry (72, 89, 93) responsive to said processing circuitry (82) to generate a pilot signal at said at least one frequency and place said pilot signal with a signal to be amplified.

8. The system of claim 7 **CHARACTERIZED BY:**

pilot detection circuitry (48, 95, 96, 97, 98, 99,

100, 103) coupled to said processing circuitry and configured to receive said pilot signal at said at least one frequency, said pilot detection circuitry producing to said processing circuitry (82) a pilot amplitude signal representing an amplitude for said pilot signal at said at least one frequency; and  
 said processing circuitry (82) gain and/or phase adjustments based on said pilot amplitude signal.

9. The system of claim 8 **CHARACTERIZED BY:**

a first splitter (14) receives a signal to be amplified and provides a replica of said signal onto a main signal path (16) and a feed forward path (18);  
 a first amplifier (12) on said main signal path (16) amplifies said signal on said main signal path (16) to produce an amplified signal with distortion and said pilot signal on said main signal path (16);  
 a first coupler (26) couples a replica of said amplified signal with said distortion and said pilot signal onto a coupling path (30);  
 a second coupler (28) combines said signal on said feed forward path (18) with said replica of said amplified signal with said distortion and said pilot signal on said coupling path (30) to produce said distortion and said pilot signal on said feed forward path (18);  
 a gain and/or phase circuit (42) on said feed forward path (18) receives said distortion and said pilot signal to adjust the amplitude and/or phase of the said pilot signal on said feed forward path;  
 a third coupler (46) combines said distortion and said pilot signal on said feed forward path (18) with said amplified signal with said distortion and said pilot signal on said main signal path (16) to output the amplified signal with distortion and said pilot signal;  
 said pilot detection circuitry (48, 95, 96, 97, 98, 99, 100, 103) receives said amplified signal with distortion and said pilot signal and detects said pilot signal after said third coupler (46); and  
 said processing circuitry (82) providing gain and/or phase adjustments based on said amplitude of said pilot signal after said third coupler (46).

10. The system of claim 9 **CHARACTERIZED IN THAT** said pilot detection circuitry includes:

a fourth coupler (48) receives said amplified signal with said distortion and said pilot signal and couples a replica of said amplified signal

with said distortion and said pilot signal onto a pilot detection path (96);  
 frequency conversion circuitry converts said pilot signal on said pilot detection path (96) to an intermediate frequency;  
 a band pass filter (99) having a center frequency at said intermediate frequency retains said pilot signal; and  
 detection circuitry (100) produces said pilot amplitude signal in response to said pilot signal at said intermediate frequency.

**11. The system of claim 10 CHARACTERIZED IN THAT** said pilot detection circuitry includes:

at least one local oscillator (LO) (95) tuned to at least one LO frequency in response to said processing circuitry; and  
 at least one mixer (98) mixes said pilot signal with said at least one LO frequency to produce said pilot signal at said intermediate frequency.

**12. The system of claim 11 CHARACTERIZED IN THAT** said pilot detection circuitry includes:

a first local oscillator (LO) (48) tuned to a first LO frequency in response to said processing circuitry (142);  
 a first mixer (156) receives said pilot signal on said pilot detection path (152) and mixes said pilot signal with said first LO frequency to produce said pilot signal at a first intermediate signal;  
 a second LO (150) tuned to a second LO frequency in response to said processing circuitry (142);  
 a second mixer (160) receives said pilot signal at said first intermediate frequency and mixes said pilot signal with said second LO frequency to produce said pilot signal at a second intermediate frequency; and  
 said bandpass filter (162) having said second intermediate frequency as said center frequency of said bandpass filter (162).

**13. A method of producing an amplified signal, said method CHARACTERIZED BY:**

determining using upstream signal information at least one frequency for a pilot signal;  
 detecting an amplitude of said pilot signal; and  
 providing gain and/or phase adjustments based on said amplitude of said pilot signal.

**14. A distortion reduction system CHARACTERIZED BY:**

processing circuitry (82) configured to receive upstream signal information and to determine at least one frequency for a pilot signal;  
 pilot detection circuitry (48, 95, 96, 97, 98, 99, 100, 103) coupled to said processing circuitry and configured to receive said pilot signal at said at least one frequency, said pilot detection circuitry producing to said processing circuitry (82) a pilot amplitude signal representing an amplitude for said pilot signal at said at least one frequency; and  
 said processing circuitry (82) providing gain and/or phase adjustments based on said pilot amplitude signal.

**FIG. 1**  
(PRIOR ART)

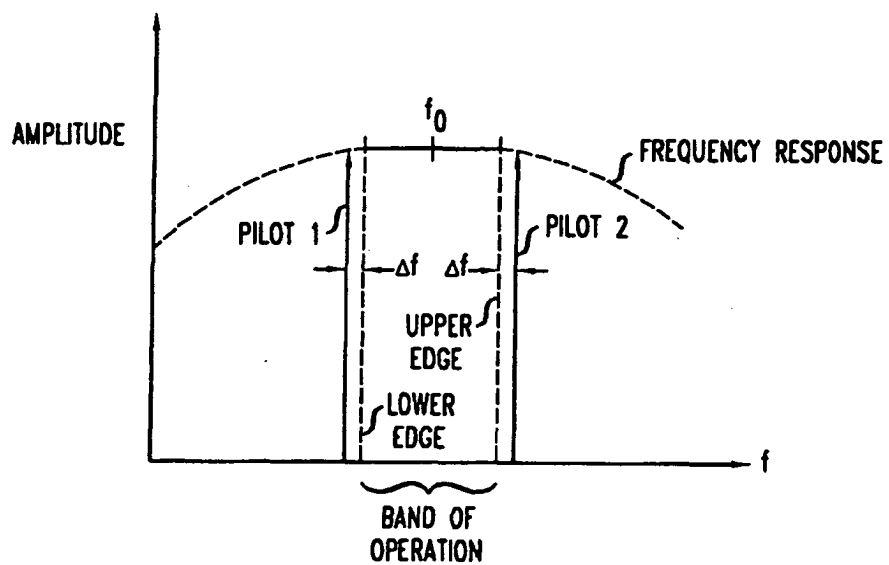
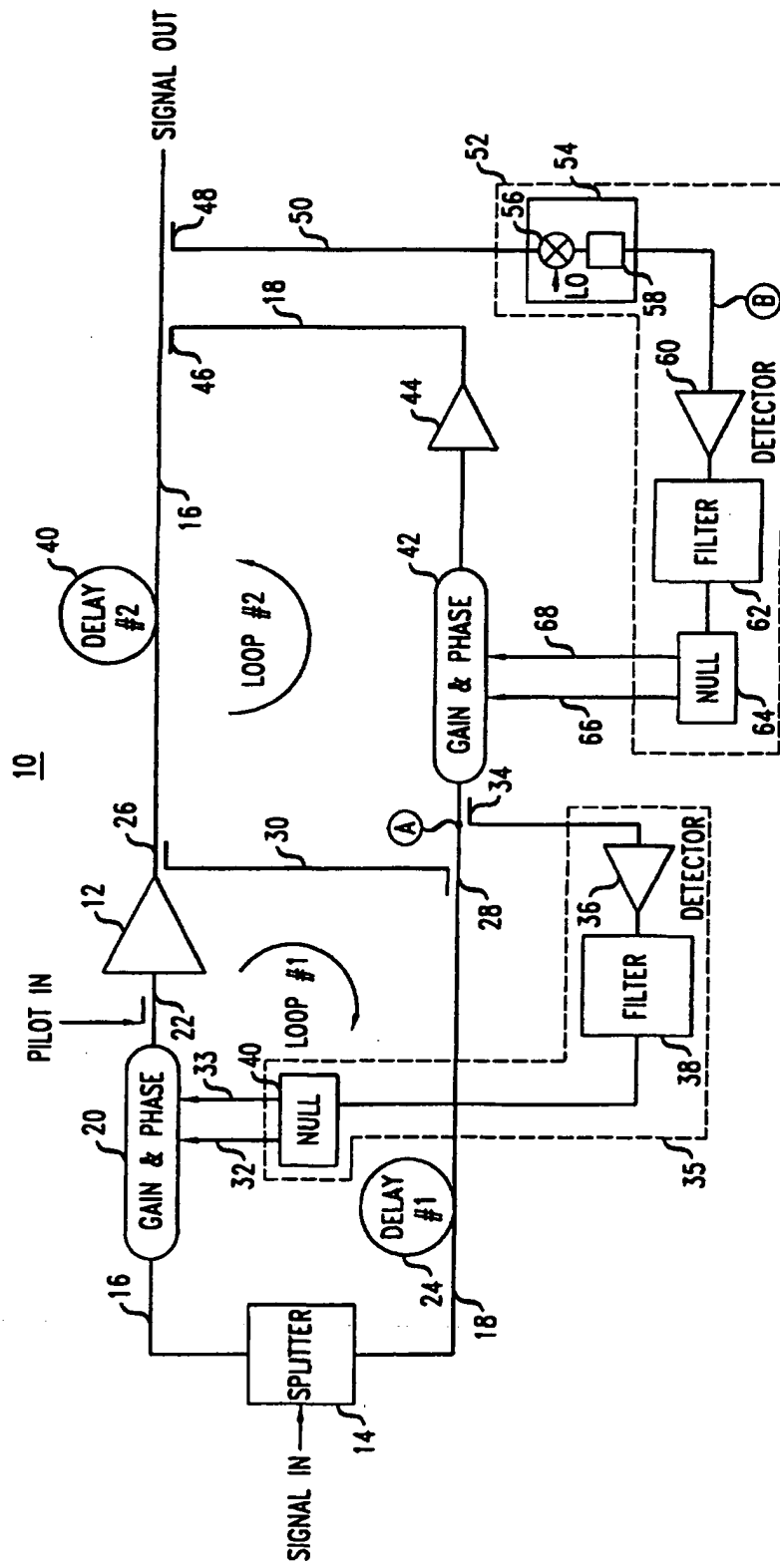


FIG. 2



**FIG. 3**

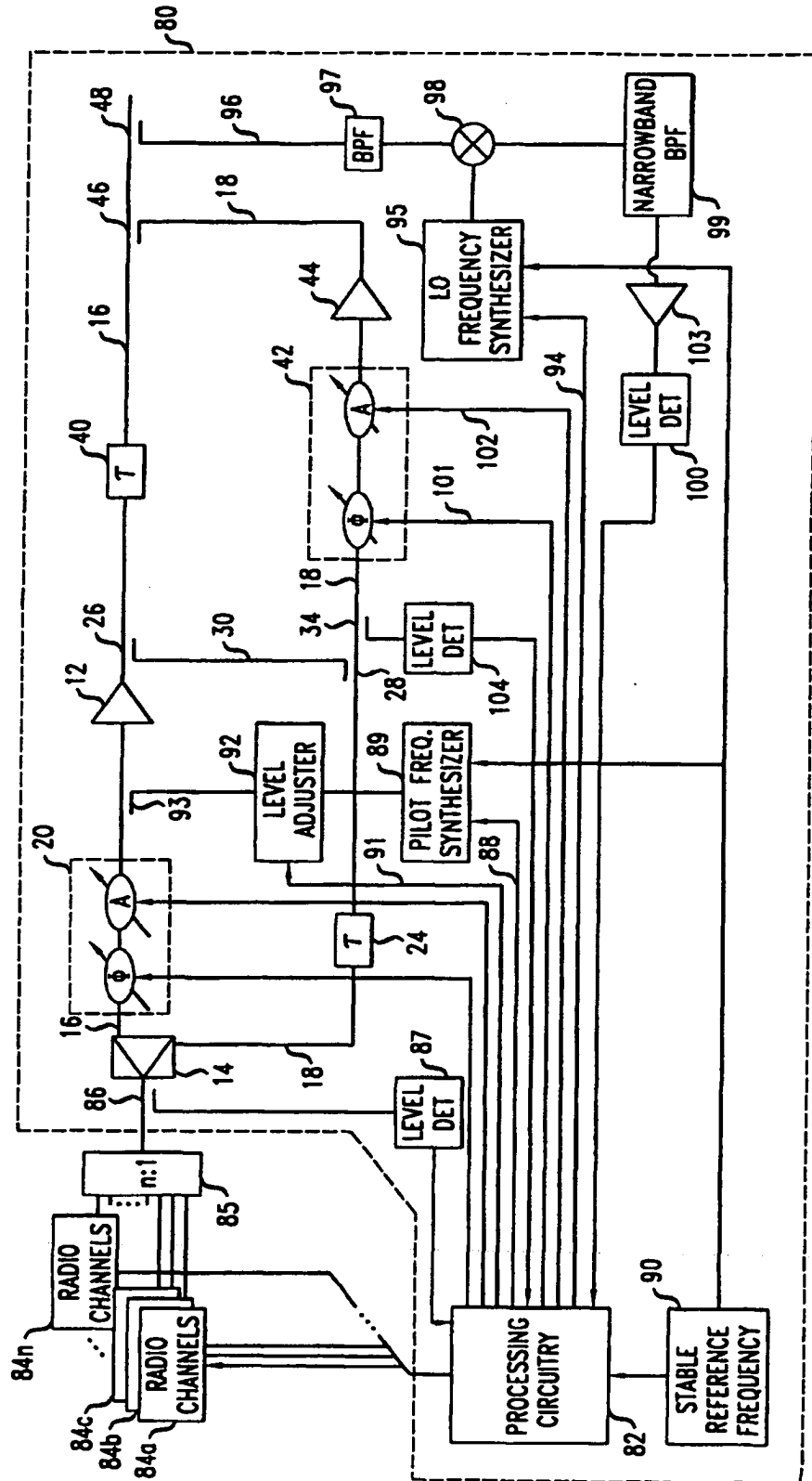


FIG. 4

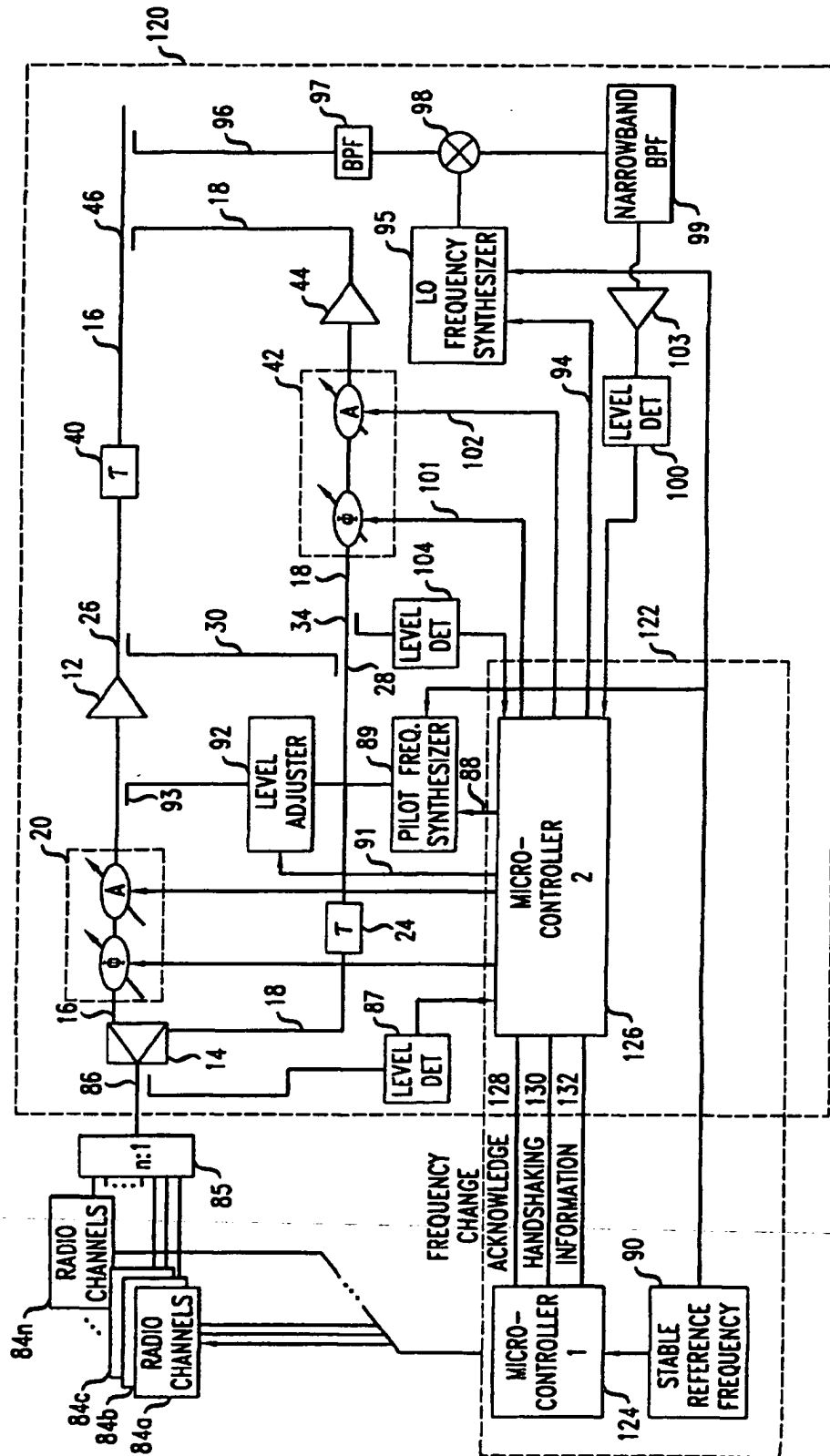
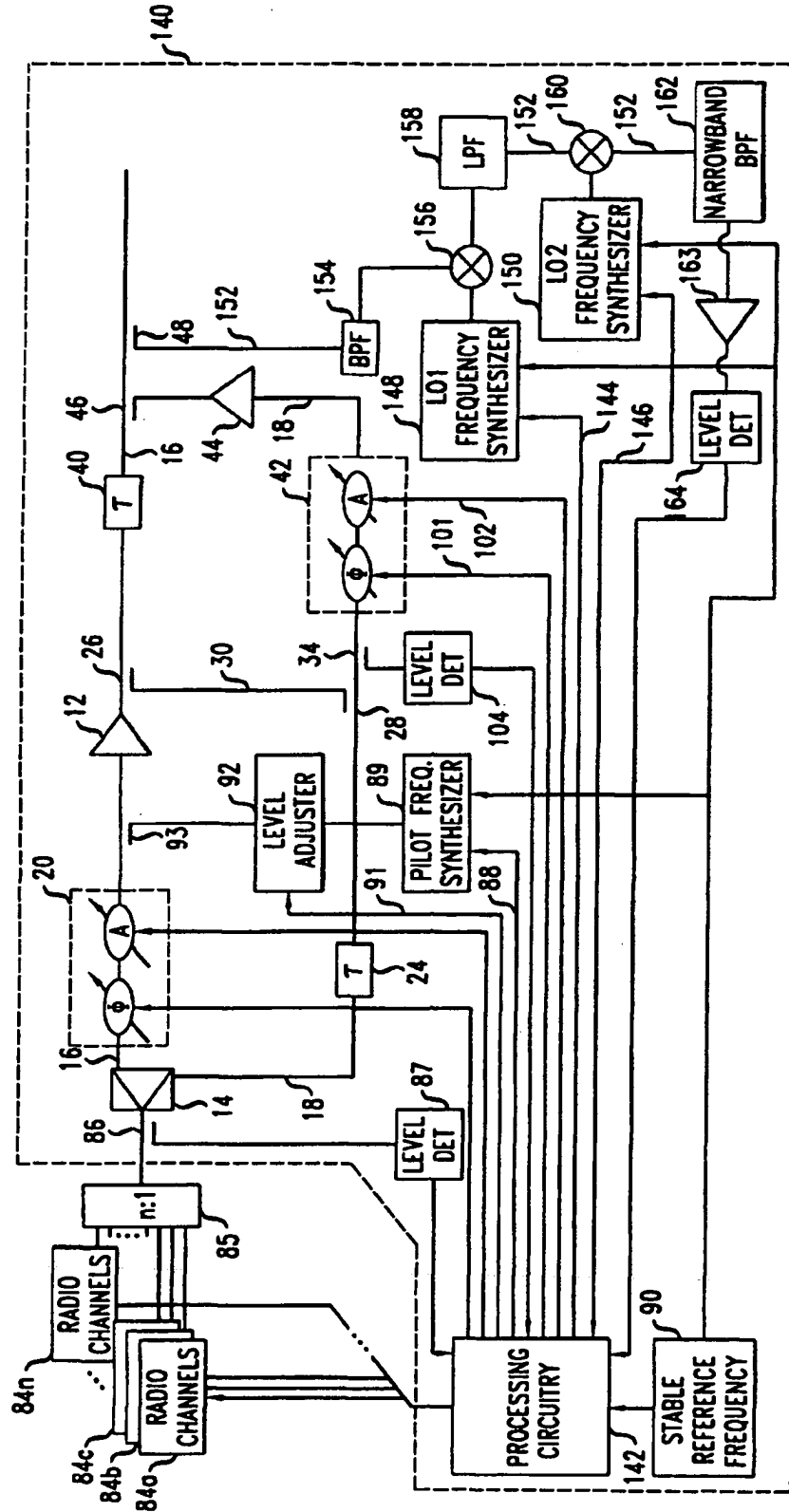


FIG. 5





**FIG. 6**

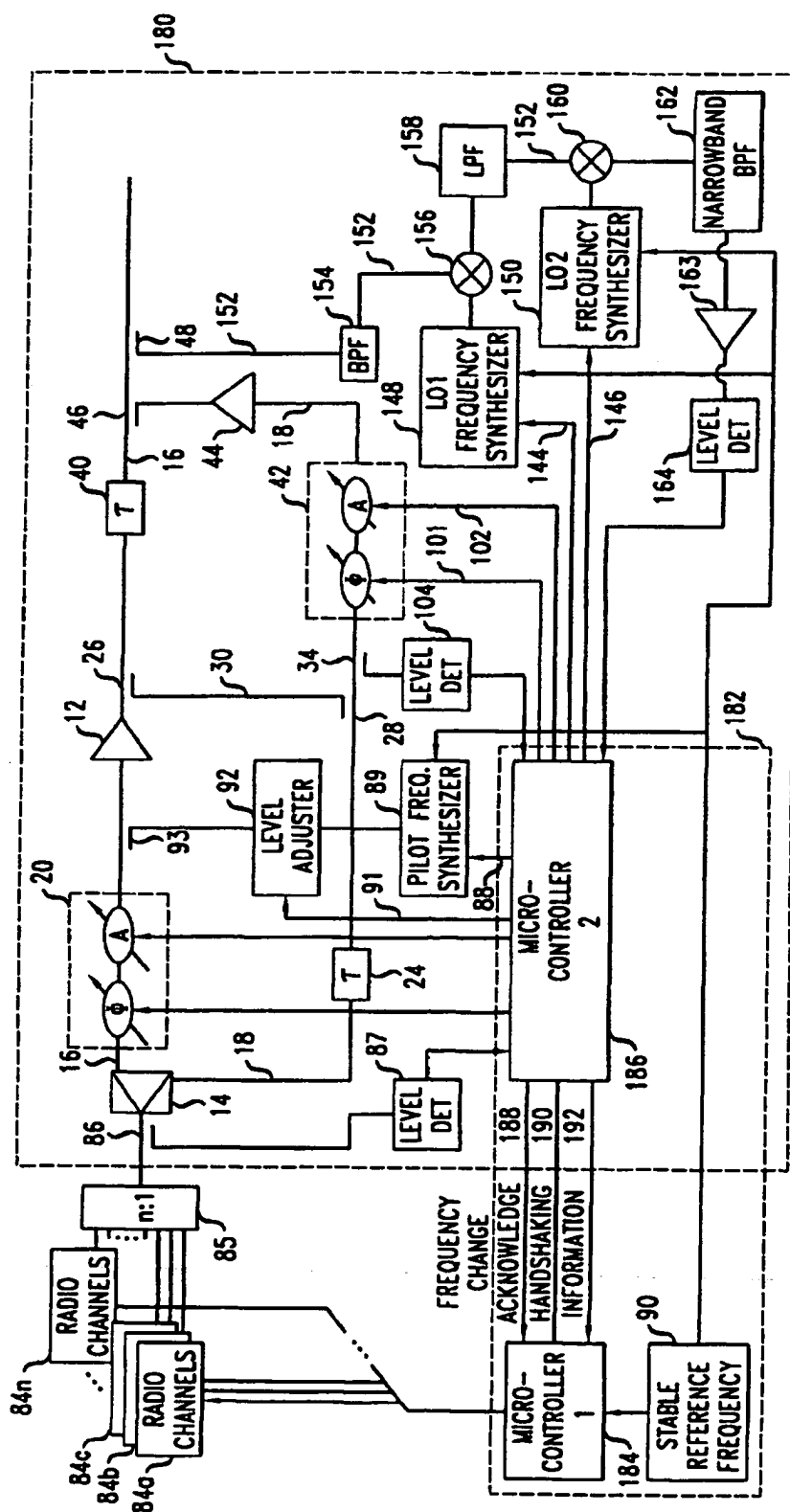
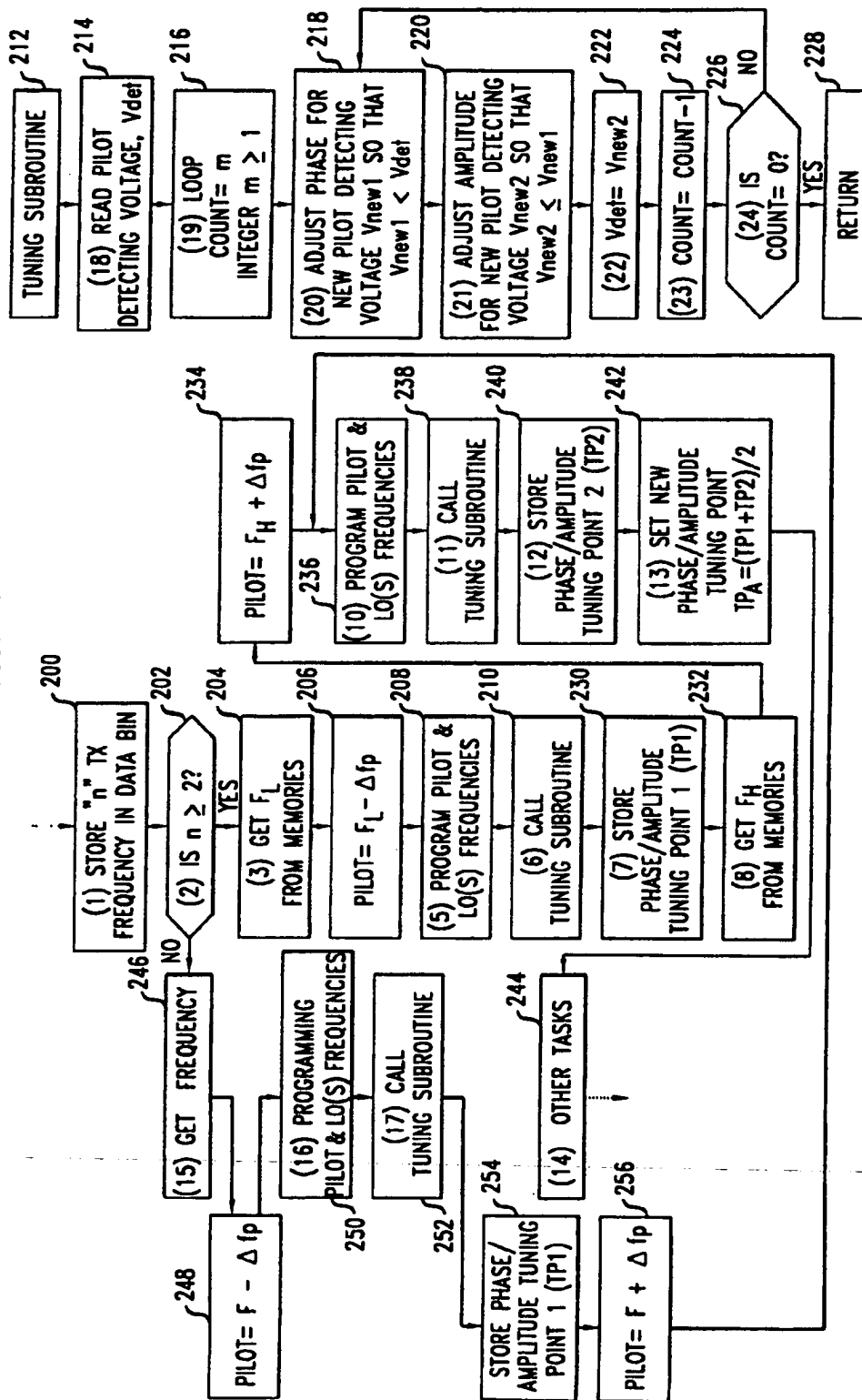


FIG. 7





European Patent  
Office

## EUROPEAN SEARCH REPORT

Application Number  
EP 01 30 1947

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The present search report has been drawn up for all claims			TECHNICAL FIELDS SEARCHED (Int.Cl.7)
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Place of search		Date of completion of the search	Examiner
THE HAGUE		17 August 2001	Segaert, P
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			

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